Interval Approach to Phase Measurements Can Lead to Arbitrarily Complex Sets – A Theorem and Ways Around It

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Abstract

We are often interested in phases of complex quantities; e.g., in non-destructive testing of aerospace structures, important information comes from phases of Eddy current and magnetic resonance.

For each measurement, we have an upper bound Δ on the measurement error $\Delta x = \widetilde{x} - x$, so when the measurement result is $\widetilde{x}$, we know that the actual value x is in $[\widetilde{x} - \Delta, \widetilde{x} + \Delta]$. Often, we have no information about probabilities of different values, so this interval is our only information about x. When the accuracy is not sufficient, we perform several repeated measurements, and conclude that x belongs to the intersection of the corresponding intervals.

For real-valued measurements, the intersection of intervals is always an interval. For phase measurements, we prove that an arbitrary closed subset of a circle can be represented as an intersection of intervals.

Handling such complex sets is difficult. It turns out that if we have some statistical information, then the problem often becomes tractable. As a case study, we describe an algorithm that uses both real-valued and phase measurement results to determine the shape of a fault. This is important: e.g., smooth-shaped faults gather less stress and are, thus, less dangerous than irregularly shaped ones.

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1 Interval Uncertainty for Real-Valued Measurements: Reminder

In most measurements, the measured quantity is a real number; see, e.g., [16].

Measurements are never 100% accurate; as a result, the measurement result $\widetilde{x}$ is usually different from the actual (unknown) value x of the measured quantity. For each measuring instrument, the manufacturer provides an upper bound Δ on the (absolute value of the) measurement error $\Delta x \stackrel{\text{def}}{=} \widetilde{x} - x$: $|\Delta x| \le \Delta$. (If no such bound is provided, this means that an arbitrarily large and/or arbitrarily small value of x is possible, so $\widetilde{x}$ is rather an estimate and not a measurement.)

Often, in addition to this upper bound, we know the probabilities of different values of Δx. However, in many practical situations, we have no information about these probabilities. In such

cases, after we performed the measurement and found the measurement result $\widetilde{x}$, the only information about the (unknown) actual value x is that x cannot differ from $\widetilde{x}$ by more than Δ – i.e., in other words, that x belongs to the interval $\mathbf{x} = [\widetilde{x} - \Delta, \widetilde{x} + \Delta]$.

Often, measurement results serve as inputs to complex data processing algorithms, algorithms that use the measurement results $\widetilde{x}_1, \ldots, \widetilde{x}_n$ to estimate the values of the quantity y that are difficult (or even impossible) to measure directly. There exists techniques – known as *interval computations* (see, e.g., [7, 9, 10, 13]) – that analyze how the interval uncertainty $\mathbf{x}_1, \ldots, \mathbf{x}_n$ in the inputs x_i propagates to the uncertainty $\mathbf{y}$ of the result y of data processing.

Sometimes, the measurement error is too large, so the accuracy resulting from a single measurement is not sufficient. In this case, a natural idea is to perform repeated measurements of the same quantity. After each measurement, we get an interval $\mathbf{x}_i$ that contains the actual value x of the measured quantity. After N measurements, we know that the value x belongs to all n intervals $\mathbf{x}^{(i)}$; therefore, the actual value x belongs to the *intersection* $\bigcap \mathbf{x}^{(i)}$ of these intervals. This intersection is always an interval, so using this intersection instead of the original (wider) interval does not increase the complexity of the corresponding data processing.

This method is not only in accordance with common sense: it can actually be proven (see, e.g., [19, 20]) that under reasonable conditions, for large N, the intersection is indeed much narrower than each of the original intervals – in other words, repeated measurements do drastically improve the measurement accuracy.

2 Phase Measurements: Necessity

In most measurements, the measured quantity is a real number; however, in many cases, the measured quantity is determined by the delay between the two waves. In such situations, it is often impossible to determine the actual delay, because if the delay coincides with the full period (2π radians), then the two waves – original and delayed one – are practically indistinguishable. In such situations, we cannot measure the actual delay, we can only measure the relative *phase* φ of the two waves, the phase that takes values from 0 to 2π in such a way that 0 and $2 \cdot \pi$ are indistinguishable. In geometric terms, we can describe the phase φ by a point on the unit circle whose radius forms an angle φ with the OX axis. Let us give two examples of phase measurements.

In Very Large Baseline Interferometry (VLBI; see, e.g., [17]), we use two (or more) distant antennas (separated by several thousand miles) to record the signal from the same extra-galactic radio source. Each antenna site is equipped with a super-precise clock, so we are able to exactly reference each observation to time and thus, to compare the times that it takes for the signal to reach the two antennas. Unfortunately, to be able to effectively amplify the signal, we must restrict ourselves to a narrow frequency band. Within this narrow band, the signal is so close to being periodic that we cannot effectively measure the actual delay between the two recorded signals – only the phase shift between these signals.

Another case when phase measurements are very important is ultrasonic testing of structural integrity; see, e.g., [4, 5]. In this testing, a transmitter emits an ultrasonic wave; part of this wave goes directly to the sensor, part is first reflected by the fault. The delay between the two detected signals indicates how far away the fault is. Similarly to the VLBI case, often, by comparing the two waves, we cannot determine the delay exactly, we can only determine the phase shift between the two waves.

In both examples – VLBI and non-destructive testing – there exist efficient methods for handling the phases. In addition to the above-cited sources, we can mention [1, 2, 3, 6, 11] for radioastronomical data processing, and [15, 21] for data processing in non-destructive testing.

3 Phase Measurements: Interval Uncertainty

Similarly to the case of real-valued measurements, phase measurements are never 100% accurate. The measurement error of a phase measurement can be described by a *distance* $d(x, \widetilde{x})$ between the actual (unknown) value of the phase x and the measured value $\widetilde{x}$. On a unit circle, this distance can be defined as the length of the shortest of the two arcs that connect the corresponding points. In analytical terms, the distance between the two values from 0 to $2 \cdot \pi$ can be defined as

$$d(x, \widetilde{x}) = \min(|x - \widetilde{x}|, |x - \widetilde{x} - 2 \cdot \pi|, |x - \widetilde{x} + 2 \cdot \pi|).$$

For example, the distance between the values 0 and 3 is equal to the smallest of 3 and $2 \cdot \pi - 3 \approx 0.14$, i.e., to 0.14.

Similar to the real-valued measurements, in many real-life situations, the only information we have about the measurement error of the phase measurement is the upper bound Δ on the distance between x and $\widetilde{x}$. In this case, once we have performed the measurement and measured the value $\widetilde{x}$, the only information that we have about the actual value x of the phase is that x belongs to the interval $[\widetilde{x} - \Delta, \widetilde{x} + \Delta]$; see, e.g., [11].

For simplicity, let us illustrate these intervals in terms of degrees (not radians); in terms of degrees, the full circle is 360°.

- If we measured the phase as $\widetilde{x} = 180^\circ$, and the upper bound on the measurement accuracy is $\Delta = 100^\circ$, then the actual value of the phase can be anywhere between $180 - 100 = 80^\circ$ and $180 + 100 = 280^\circ$.
- If we measured the phase as $\widetilde{x} = 0^\circ$, and the upper bound on the measurement accuracy is $\Delta = 100^\circ$, then the actual value of the phase can be anywhere between $0 - 100 = -100^\circ = 260^\circ$ and $0 + 100 = 100^\circ$. In terms of angles from 0 to 360, this interval goes from 260 to 360 (which is the same as 0) and then from 0 to 100.

Similarly to the real-valued measurements, if we are not satisfied with the accuracy of a single measurement, a natural idea is to perform repeated measurements of the same quantity and then take the intersection of the corresponding intervals. For real-valued measurement, this intersection is always an interval. In contrast, for phase measurements, the intersection of two intervals may no longer be an interval. Indeed, for the above two measurements, the intersection of the intervals

$$[180 - 100, 180 + 100] = [80, 280]$$

and

$$[0 - 100, 0 + 100] = [-100, 100] = [260, 360] \cup [0, 100]$$

is not a single interval, but a union of two disjoint intervals: $[80, 100]$ and $[260, 280]$.

How complex can such an intersection be?

4 How Complex Can Such an Intersection Be?

We have already seen that the intersection of two intervals can consist of two disjoint intervals. If we add the third interval $[270 - 175, 270 + 175]$ to the above intersection, we conclude that the triple intersection consists of three disjoint intervals: $[260, 265]$, $[275, 280]$, and $[80, 100]$. Our main result is that this intersection can be arbitrary complex:

Theorem. *An arbitrary closed subset of a circle can be represented as an intersection of intervals.*

Restriction to closed sets is necessary because each interval is a closed set, and the intersection of closed sets is always close. So, this theorem says, in effect, that the interval approach to phase measurements can lead to arbitrary complex sets.

Comment. The fact that taking interval uncertainty into consideration leads to an increase in complexity is in line with other similar situations; see, e.g., [12].

Proof. Let S be a closed subset of a unit circle C. Then, its complement $-S$ is an open set (see, e.g., [8]). By definition, an open set contains, together with each of its points α, an open ball I_α. On a circle with the above-defined metric d, an open ball is an open interval, so for every point $\alpha \in -S$, there exists an open interval $I_\alpha \subseteq -S$ for which $\alpha \in I_\alpha$.

- Since each of the open intervals I_α is contained in the set $-S$, the union $\bigcup I_\alpha$ of these open intervals is also a subset of $-S$: $\bigcup I_\alpha \subseteq -S$.
- Since every element α of the set $-S$ belongs to the corresponding open interval I_α and therefore, belongs to their union, we can also conclude that $-S$ is a subset of the union $\bigcup I_\alpha$: $-S \subseteq \bigcup I_\alpha$.

Thus, the complement $-S$ is equal to the union $\bigcup I_\alpha$ of the open intervals I_α.

Due to de Morgan's laws, we can now conclude that

$$S = -(-S) = -\left(\bigcup_\alpha I_\alpha\right) = \bigcap_\alpha (-I_\alpha).$$

On a circle, a complement $-I_\alpha$ to an open interval is a closed interval. Therefore, the set S can indeed be represented as an intersection of closed intervals. The theorem is proven.

Comment. In this proof, we represent a closed set as an intersection of continuum many open intervals; if we restrict ourselves to rational values α, we will be able to get a similar representation with no more than countably many intervals.

5 What Can We Do: Case Study

In the previous section, we have proved that an arbitrary (in particular, arbitrarily complex) closed subset of a circle can be represented as an intersection of intervals.

Handling such complex sets is difficult. It turns out that if we have some statistical information, then the problem often becomes tractable.

5.1 Shape Detection and Why It Is Important

As a case study, we describe an algorithm that uses both real-valued and phase measurement results to determine the shape of a fault; see [14] for details. This shape detection is important: e.g., smooth-shaped faults gather less stress and are, thus, less dangerous than irregularly shaped ones.

Detecting shapes of faults is useful in other applications as well; for example:

- in military applications, we want to be able to distinguish between a tank and a heap of rubbish;

- in medical imaging, we must be able to detect the shapes of skin formations: regularly shaped formations are mostly harmless, but the irregularly shaped ones could mean cancer.

As a test case, we used a benchmark B-52 plate provided by Boeing which contains 16 artificially induced smooth-shaped (circular) and angular-shaped (square) faults of 4 different sizes both inside and on the edge: 4 inside squares of sizes $1/2'' \times 1/2''$, $3/8'' \times 3/8''$, $1/4'' \times 1/4''$, and $1/8'' \times 1/8''$, 4 edge squares of the same sizes, 4 inside circles with diameters $1/2''$, $3/8''$, $1/4''$, and $1/8''$, and 4 edge circles of the same diameters. Seven different measurements were done on this plate: two Pulse Echo measurements at different frequencies, four measurements of magnetic resonance, and one measurement of Eddy current. Six of these 7 measurements measure phase (Eddy current is the only exception).

None of these 7 measurements detects all the faults; e.g., Eddy current only detects circular faults, etc. We therefore need to combine ("fuse") the results of these measurements. Several such fusion methods have been proposed [5]; the best of the known fusion methods is the following one (see [15] for more detail).

5.2 Existing Methods of Fault Detection and Why They Are Not Perfect for Shape Reconstruction

This method is based on the fact that faults can be detected by unusual values of different measured quantities; in statistical terms, we can say that faults can be detected as *outliers*. For each plate, and for each measurement type x_i, the probability distribution of measurement result for regular (non-fault) points is close to Gaussian; as a result, we can detect an outlier as a point A for which $x_i(A)$ is outside the corresponding 2 sigma interval (or 3 sigma), i.e., for which $|x_i(A) - a_i| > 2 \cdot \sigma_i$, where a_i and σ_i are the mean and standard deviation of the corresponding Gaussian distribution.

How can we compute the values a_i and σ_i? If we had a plate with no faults, then we could simply compute a_i as the average of all the values $x_i(a)$, and, accordingly, σ_i as $\sqrt{(1/N) \cdot \sum_A (x_i(A) - a_i)^2}$, where N is the total number of pixels. However, the whole point is that there are faults, and if we take the average of all the values $x_i(a)$, including the fault points A, we get a biased estimated for a_i. To avoid this bias, we can apply an *iterative* method in which we sequentially re-calculate the values a_i and σ_i and also mark points as possible outliers. At first, none of the points are marked. At each step, we:

- compute the new value of a_i as the average of $x_i(A)$ over all un-marked points, and then compute σ_i as $\sqrt{(1/N) \cdot \sum_A (x_i(A) - a_i)^2}$, where N is the total number of un-marked points;
- then, we additionally mark points for which $|x_i(A) - a_i| > 2 \cdot \sigma$ as outliers.

We stop when no new points are marked.

Based on the resulting estimates of a_i and σ_i, we compute, for every measurement i and for every pixel A, the normalized value $z_i(A) \stackrel{\text{def}}{=} (x_i(A) - a_i)/\sigma_i$. According to normal distribution, the probability that a non-fault point A has value $z_i(A)$ is proportional to $\exp(-(z_i(A))^2)$.

It is reasonable to assume that the measurement results x_i and x_j are statistically independent (if x_j was strongly dependent on x_i, then measuring x_j would not make much sense after we have already measured x_i). In this case, the normalized values are also independent, and so the probability for a non-fault point to have values $(z_1(A), \ldots, z_n(A))$ is proportional to

$$p = \prod_{i=1}^{n} \exp(-(z_i(A))^2) = \exp\left(-\sum_{i=1}^{n} (z_i(A))^2\right).$$

If this probability is very small (smaller than a certain threshold p_0), then this point cannot be a regular point and is, therefore, an outlier. Turning to logarithms, we can transform the criterion $p \le p_0$ into an equivalent form $\sum(z_i(A))^2 \ge t_0$ for some new threshold t_0. Since we have already selected a 2 sigma criterion for outliers – a criterion in which 5% of the normally distributed points can be misclassified as outliers, it is reasonable to accept a similar 5% criterion for selecting the value t_0. This leads to a $t_0 = n \cdot (1 + 2 \cdot \sqrt{2/n})$. So, we mark a point A a fault if the sum $\sum(z_i(A))^2$ exceeds this threshold t_0.

To make this algorithm work better, we need to make two minor modifications:

- First, we have to process edges separately and the interior of the plate separately. Reason: faults are points where the plate is thinner; near the edges, it is also thinner, so if we combine the edge pixels with the interior ones, then the entire edge will show as one big fault.
- Second, some of the outlier values $x_i(A)$ are caused by a malfunctioning of the measuring instrument. To avoid marking such points as outliers, we mark a point as fault only if, in addition to $|z_i(A)| > 2$, at least one more mode $j \ne i$ detects an outlier either at this very point A or at some point B in the nearest neighborhood of this point A (i.e., for which $\rho(A, B) \le c$ for some small $c > 0$). If for all other measurements $j \ne i$ in this small neighborhood, we have $|z_j(B)| \le 2$, we dismiss the value $z_i(A)$ as a probable malfunctioning of the measuring instrument. For this pixel, we thus combine only 6 remaining values $z_j(A)$ $(j \ne i)$ instead of the usual seven.

Figure 1: Existing Method

On a test plate and on several other plates with known fault locations, the resulting method detects the faults very well, in the sense that it has the smallest number of false positives (regular points erroneously marked as faults) and false negatives (fault points erroneously marked as regular). However, the *shape* of the reconstructed set of fault points is not reproduced well: some square faults look like circles and vice versa.

5.3 New Method Which Is Better for Shape Detection

The main reason why the existing method is not very good in detecting shape in that in the existing method, our main objective was not to miss any faults – because faults are dangerous. Therefore, when there was good evidence to support both hypotheses: that the pixel A is a fault and that the pixel A is not a fault – we tended to declare it a fault. As a result, we "padded" the set of fault points with extra points – thus distorting the shape of the set of all the fault points.

To get the shape better, it is therefore reasonable to treat the two hypotheses equally. Specifically, we consider two hypotheses: H_0 that a point is not a fault and H_1 that the point is a fault, and we use the standard techniques of hypothesis testing (see, e.g., [18]) to decide which of these hypotheses is more probable: we choose H_1 if the ratio p_1/p_0 of the probability of H_1 to the probability of H_0 exceeds a certain threshold t.

We already know how to describe the probability of H_0. It turns out that the distribution of $z_i(A)$ for fault points is also approximately Gaussian – of course, with different values a_i^f and σ_i^f. (We can estimate the values a_i^f and σ_i^f by processing the points that are marked as outliers after the iterative algorithm for computing a_i and σ_i.) As a result, after taking logarithms of both sides, we can transform the criterion $p_1/p_0 \geq t$ to an equivalent form

$$\sum_{i=1}^{n} \left((z_i(A))^2 - \left(\frac{z_i(A) - a_i^f}{\sigma_i^f} \right)^2 \right) \geq t_0.$$

Same arguments as before lead us to choose the same value for t_0.

Minor point: to apply this algorithm, we need to have enough fault point to be able to conclusively estimate a_i^f and σ_i^f; there were enough such point in the interior of the plate, but not enough on the edge; so, we only applied this method in the interior.

As a result, we got a better shape reconstruction. Specifically, to estimate the quality of the shape reconstruction of a square fault, we took the set F of all the points marked as faults in the neighborhood of an actual fault, found the square S that is the closest to the resulting set (in the sense that the total number of pixels in the symmetric set difference is the smallest), and then estimates the number of false positives and false negatives by comparing F and S. Similarly, for circular faults, we compare the set F with the closest circle C. Then, we take the total number of false positives over all 8 inside faults, and the total number of false negatives over these faults. Here is the result of our comparison:

- When we apply this procedure to the original method from [15], we got 2,443 false positives and 19 false negatives inside the plate.
- For the new method, we got 1,895 false positives and 11 false negatives inside the plate.

Conclusion: the new method is indeed much better in reconstructing shapes.

Figure 2: New Method

5.4 How Are These Results Related to Our Theorem?

The new method is better in reconstructing shapes, better but not perfect. Can we make it perfect? What the theorem says is that perfect data analysis is computationally difficult, so, most probably, we cannot expect a perfect method.

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