The background of the slide features the official seal of the University of Texas at El Paso. The seal is circular and contains a central five-pointed star. Above the star is a landscape with a river and mountains, and below it is a smaller five-pointed star. The words "UNIVERSITY OF TEXAS" are written in an arc at the top, and "AT EL PASO" is written in an arc at the bottom. The seal is rendered in a light, semi-transparent gold color.

Department of Geological Sciences

---

**Backcalculation of Intelligent Compaction Data for the  
Mechanical Properties of Soil Geosystems**

Afshin Gholamy

November 14, 2018



- **Formulation Of The Problem**
- **Inverse Problem for Intelligent Compaction: Results**
- **Auxiliary Tasks**
  - ▶ Elastic Modulus Formula: Theoretical Explanation
  - ▶ Safety Factors in Soil and Pavement Engineering
  - ▶ How Many Monte-Carlo Simulations Are Needed?
  - ▶ Why 70/30 Training/Testing Relation?
  - ▶ How to Minimize Relative Error?
  - ▶ How to Best Apply Neural Networks in Geosciences?
  - ▶ What Is the Optimal Bin Size of a Histogram?
- **Conclusions**

# *Part One*



---

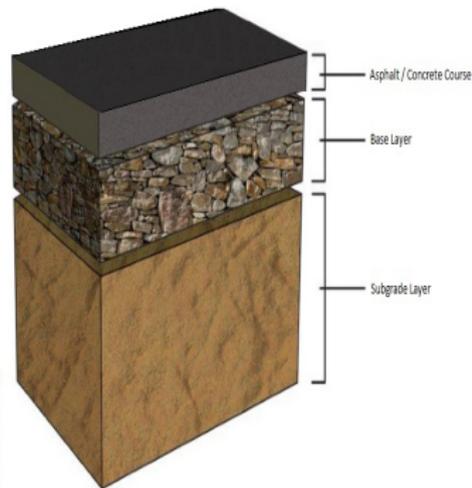
## Formulation of the Problem

## Need to Determine Mechanical Properties of Earthworks During Road Construction

- For national economy, it is very important to have a **reliable infrastructure**. So, all over the world, roads are being built, maintained, expanded, and repaired.
- Building a good quality road is very expensive, it costs several million dollars per mile. It is therefore crucial to make sure that the road lasts for a long time.
- The road is built on top of the soil.
- Soil is rarely stiff enough, so usually, the soil is first compacted.
- If needed, stiffening materials called stabilizers (or treatments) are added to the soil before compaction.



- The layer of original soil is called **subgrade**.
- On top of the subgrade, additional stiff material is placed, which is referred to as the **base** layer.
  - ▶ Base is usually composed of granular material.
  - ▶ This layer is also compacted, to make it even stiffer.
  - ▶ The base is typically reasonably thick: **15 - 30 cm**.
- It is difficult to compact a layer of such thickness, so usually, practitioners:
  - ▶ Place first a thinner layer of the base material, compact it, then
  - ▶ Place another thinner layer, etc., until they reach the desired thickness.
- Finally, **asphalt** or **concrete layer** is placed on top of the base.





## Practical Problem

- For the road to be of high quality, all three layers must be sufficiently stiff.
- Current methods of estimating the stiffness are time/labor-consuming.
- A more accurate technique is:
  - ▶ Take a sample from the compacted subgrade or base, and
  - ▶ Bring it to the lab, and measure the mechanical parameters that characterize the corresponding stiffness.
- Since most roads are built in areas which are far away from the nearby labs, this procedure usually takes days.



## Practical Problem (cont-d)

- While the road is being tested, the road-building company have two alternatives:
  - ▶ Keep the road building equipment idle – which will cost money, or
  - ▶ Move it to a new location, in which case there is a risk that we will need to move it back.
- To minimize this risk, companies usually over-compact the road – which also leads to additional costs.
- Another possibility is to measure the road stiffness on-site.

- There are several on-site measuring techniques: LWD, FWD, DCP, NDG, PLT, etc.
- All these techniques are very labor-intensive, and take days to acquire and process the data.
- Besides, in contrast to the lab measurements:
  - ▶ These techniques do not directly measure stiffness/modulus,
  - ▶ They measure density and other parameters based on which we can only make *approximate estimates* of the desired road stiffness.



- In addition, all the existing methods – both lab-based and on-site – are **Spot tests**.
- They only gauge the road stiffness at certain points.
- Thus, if the road has a relatively small **weak spot**, these methods may not detect it.
- And, based on these methods, we may erroneously certify this road as ready for exploitation.
- Such a faulty road may soon require costly maintenance – at the taxpayers' expense.



## Main Idea:

- We measure the road's mechanical properties while the road is being compacted by a roller.
- This can be done by placing:
  - ▶ Accelerometers on the rollers and/or
  - ▶ Geophones at different depths in several locations.
- Based on the results of these measurements, we can determine the mechanical properties of the road.



- The relation between the mechanical properties of the soil and the resulting accelerations is very complex.
- It is described by a **system of dynamic non-linear partial differential equations**. Even in an ideal situation:
  - ▶ When we know all the mechanical characteristics of the subgrade and of the base,
  - ▶ It takes several hours on an up-to-date computer to find the corresponding accelerations.
- We want to perform **back-calculation** (*inverse algorithm*) to determine the mechanical characteristics of the soil system from the accelerations.
- In this dissertation, we develop a method for determining the *desired characteristic in real time*.

- 1 **For the single-layer (subgrade) case**, we need to:
  - ▶ Determine the corresponding characteristics of stiffness based on the *acceleration measurements*.
- 2 **For the two-layer (subgrade + base) case**, once we have started compacting the base, we need to:
  - ▶ Determine the mechanical characteristics of the base layer based on the *measured acceleration* and on the *already-determined* characteristics of the subgrade.

Let us explain, in detail, what is needed for these tasks.

- A similar problem has been studied in the analysis of earthworks related to buildings, bridges, dams, etc., however, road-related problems are different.
  - ▶ In building construction, we have a reasonably *constant stress* on the underlying soil.
  - ▶ In contrast, for road construction, we have a *fast-changing stress* when a vehicle goes over this section of the road.
- To capture the effect of such dynamic loads, engineers developed a special notion of **elastic Modulus** (E).
- So, we need to estimate the elastic modulus in both layers at different locations.

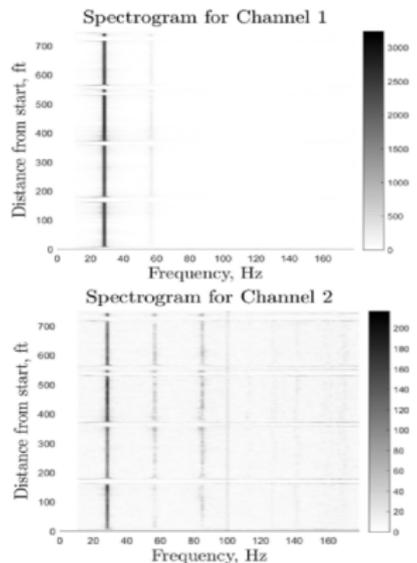
- Usually, the parameters  $k'_2$  and  $k'_3$  are determined by the material – whether it is clay or gravel. In contrast, the parameter  $k'_1$  varies strongly even for the same material.

### For example:

For *granular materials*, the value of  $k'_1$  depends on the size and shape of the grains, their density, etc. Thus:

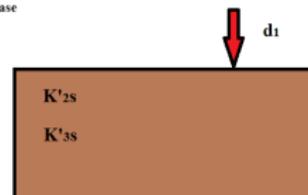
- ▶ Once we know the substance forming the soil and/or material used for the base layer,
  - ▶ We know the corresponding values  $k'_2$  and  $k'_3$  but not the corresponding values of  $k'_1$ .
- To enhance compaction, the roller vibrates with a frequency between 20 - 40 Hz.
  - So, the whole process is periodic with this frequency.

- The measured acceleration is also periodic with the same frequency.
- So, to approach this problem, it is reasonable:
  - ▶ To perform a **Fourier transform**, and to keep only the components corresponding to this known frequency.
- The resulting information can be equivalently described in terms of the **displacement (d)**.

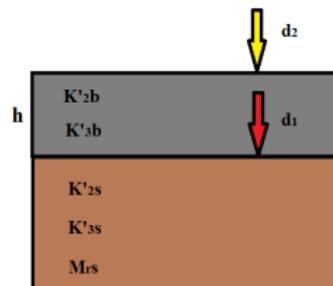


- From this viewpoint, we face the following two tasks:
  - Task 1 (Single-layer case):** Determine the elastic modulus  $E$  based on  $d_1$ ,  $k'_{2s}$ , and  $k'_{3s}$ .
  - Task 2 (Two-layer case):** Determine the elastic modulus  $E$  of the base layer from  $d_1$ ,  $d_2$ ,  $k'_{2b}$ ,  $k'_{3b}$ ,  $k'_{2s}$ ,  $k'_{3s}$  and the resilient modulus of the subgrade  $M_{rs}$ .

Single-layer case



Double-layer case





# Physics-Based Approach vs. Soft Computing Approach

- We need fast techniques for solving these two problems. Therefore, we need simple expressions for the corresponding solutions.
- There are two ways of getting such expressions:
  - ① A traditional idea is to use the corresponding **physics** to come up with possible terms.
  - ② An emerging approach is to let the computers find the terms which are empirically most appropriate.
- In our research, we use both approaches and select the best of the resulting models.

- A challenge is that the usual mechanical equations use different mechanical characteristics:
  - ▶ Principal stresses  $\sigma_1$ ,  $\sigma_2$ , and  $\sigma_3$ ;
  - ▶ The *bulk stress*  $\theta = \sigma_1 + \sigma_2 + \sigma_3$ ,
  - ▶ The *octahedral shear stress*

$$\tau_{\text{oct}} = \frac{1}{3} \sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_1 - \sigma_3)^2 + (\sigma_2 - \sigma_3)^2}.$$

- We thus need to know how  $E$  depends on  $\sigma_i$ . Empirically the best model is Ooi's formula:

$$E = k'_1 \left( \frac{\theta}{P_a} + 1 \right)^{k'_2} \left( \frac{\tau_{\text{oct}}}{P_a} + 1 \right)^{k'_3}.$$

- We want to make sure that we are not missing a more accurate expression, thus it is desirable to have a **theoretical justification** of Ooi's formula.

### Relative Error Minimization

- Most back-calculating techniques are designed for problems where the range is small.
- In such cases:
  - ▶ To gauge the accuracy of the model, it is reasonable to simply take the difference between the actual and predicted values.

$$||E(\text{actual}) - E(\text{predicted})||$$

- In pavement engineering, the elastic modulus can change by orders of magnitude.
- **For example**, the subgrade can vary between an stiff granular soil to a very soft clay.

- In such situations:
  - ▶ Large values corresponding to stiff materials will dominate, and
  - ▶ The small differences corresponding to an important case of soft subgrade will be ignored.
- It is more appropriate to use **relative errors**, i.e., approximation errors described in terms of percentages.
- In principle, we could re-write the existing software packages so that they take into account relative error.
  - ▶ This is time-consuming.
  - ▶ Some of these packages are proprietary, they do not allow to modify their code.
- It is desirable to use the **absolute-error** techniques to minimize relative errors.

## Optimal Bin size of Histogram

- For engineers and practitioners to be able to use and understand the results, it is desirable to **visualize** them.
- Most of the estimates and predictions are probabilistic in nature.
- Thus, we need to plot the **histogram**, to give the user a clear understanding of the probabilities.
  - ▶ **Small bin size**, results in chaotic histogram, and does not give us a good understanding.
  - ▶ **Large bin size**, provides us with a good general picture, but we may miss important details.
- We thus need to select **optimal bin size**.



- In probability and statistics, there are methods of selecting optimal bin sizes.
- However, these methods assume that we already have a lot of information about the probability distribution.
- In our problem, as in many other engineering tasks, we do not have this information.
- It is thus necessary to come up with a general technique for selecting the **optimal bin size** for a histogram.



## Auxiliary Tasks: Summary

- **Task 3:** Find a theoretical justification for Ooi's empirical formula describing the resilient modulus.
- **Task 4:** Provide a theoretical justification for the empirical safety factor.
- **Task 5:** Determine the appropriate number of simulations.
- **Task 6:** Come up with the most adequate division into training, testing, and validation sets.
- **Task 7:** Solve relative-error minimization problems.
- **Task 8:** Come up with neural network techniques which are most adequate for our data processing problems.
- **Task 9:** Come up with a general technique for selecting the optimal bin size for a histogram.

# *Part Two*



## Inverse Problem for Intelligent Compaction: Main Results



# Inverse Problem for Intelligent Compaction: Reminder

- Our **main objective** of this research is to develop methods for timely evaluation of the pavement quality.
- We are considering a typical case of a pavement consisting of two layers:
  - the subgrade and
  - the base (placed over this subgrade).
- First, the subgrade is reinforced (if needed) and then compacted.
- Then, the base is placed on top of the subgrade, and the pavement is compacted again.
- On each of these two compaction stages, sensors (accelerometers) are placed on the rollers.



# Inverse Problem for Intelligent Compaction: Reminder

- The accelerations measured by these sensors are then used to gauge the **quality of the pavement**.
- A good quality pavement should have:
  - a sufficiently stiff subgrade and
  - a sufficiently stiff base.
- It is important to make sure that:
  - the pavement is stiff enough, and
  - the stiffness is uniform.
- Otherwise, the traffic load will be unequally distributed.
- This will lead to too much stress (and earlier wear) for some locations.
- For the subgrade, its stiffness can be extracted directly from the “**pre-mapping**”.



# Inverse Problem for Intelligent Compaction: Reminder

- The **stiffness of the subgrade** at each spatial location can then be determined by dividing:
  - the known force of the roller
  - by the deflection  $d_1$  at this particular location which can be determined from the sensors attached to the compacting roller.
- The **stiffness of the base** in contrast, cannot be determined directly from the measurements.
- From the sensors attached to the roller that compacts the 2-layer pavement, we can extract the deflection  $d_2$ .

- For each spatial location, we need to evaluate the stiffness of the base from:
  - the 2-layer deflection  $d_2$  and
  - the deflection  $d_1$  that describes the stiffness of the subgrade.
- We can use our knowledge of materials used for the base and the subgrade layers to determine the parameters  $k'_2$  and  $k'_3$ .
- To gauge the quality of the pavement, it is desirable to use the **“average” (representative) modulus**.
- A reasonable idea is therefore to use the modulus at half-depth of the base.



# Our General Approach to Solving the Inverse Problem

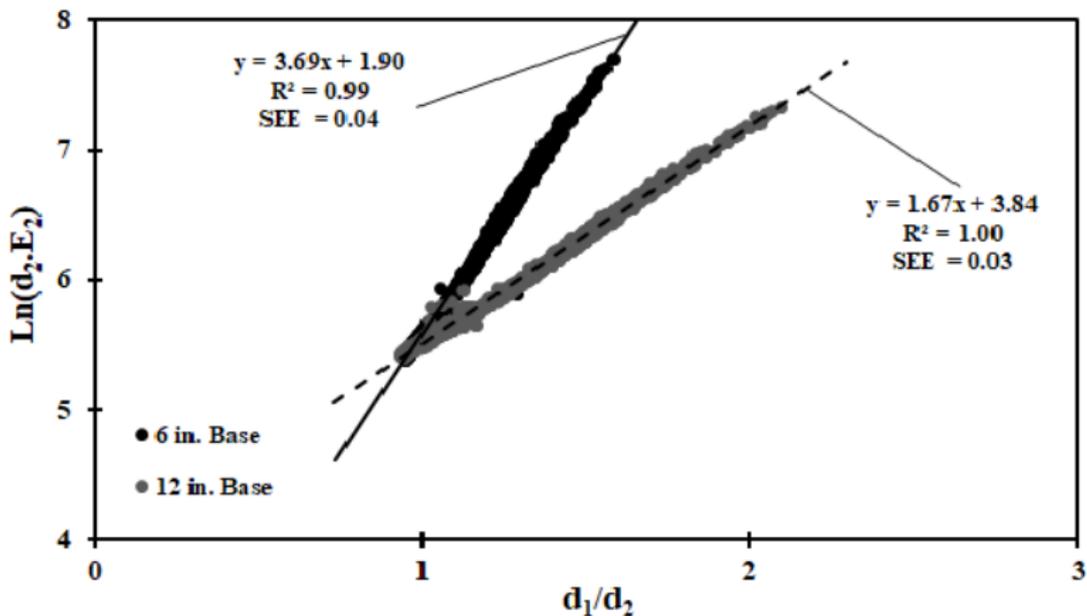
- **To test different methods** of solving the inverse problem, we used **simulations of the forward problem** for the *1-layer* and *2-layer* case.
  - We started with linear static models where the modulus is assumed to have the same value within each layer.
  - Next, we used non-linear static models in which the modulus depends on depth.
  - Finally, we used dynamical simulations.

- For the 1-layer case, we only have the subgrade.
  - The Elastic modulus  $E_1$  can be estimated based on the deflection  $d_1$ :  

$$E_1 = \frac{c}{d_1}, \text{ for a constant } c \approx 209.$$
- In the static linear 2-layer case, the modulus  $E_2$  can be obtained by the following formula:

$$E_2 = \frac{1}{d_2} \cdot \exp \left( a(h) + (\ln(c) - a(h)) \cdot \frac{d_1}{d_2} \right).$$

- In this formula,  $c = 209$ , and the coefficient  $a(h)$  depends on the thickness  $h$  of the base:
  - for  $h = 6$  inches, we have  $a(h) = 1.89$ ;
  - for  $h = 12$  inches, we have  $a(h) = 3.82$ ;
  - for  $h = 18$  inches, we have  $a(h) = 4.66$ .



- In the static stationary nonlinear case, we need to find the  $E$  of the base based on the following information:
  - the thickness of the base layer  $h$
  - the displacement  $d_2$  of the 2-layer pavement;
  - the values  $k'_{2b}$  and  $k'_{3b}$  corresponding to the base; and
  - the information about the subgrade.
- In the ideal case, we have as much information as possible about the subgrade; namely:
  - the displacement  $d_1$  of the subgrade; and
  - the values  $k'_{2s}$  and  $k'_{3s}$  corresponding to the subgrade.
- For this case, we have come up with the following formulas.

- For the **150 mm** cases, we have

$$\begin{aligned}
 \ln(d_2 \cdot E) &= 2.098 + 0.361 \cdot k'_{2b} + 0.336 \cdot k'_{3b} + 0.093 \cdot k'_{2b} \cdot k'_{3b} + 0.053 \cdot (k'_{3b})^2 \\
 &+ 0.467 \cdot (k'_{2s}) - 0.305 \cdot (k'_{2s})^2 - 0.264 \cdot k'_{2s} \cdot k'_{3s} - 0.079 \cdot (k'_{3s})^2 \\
 &+ 0.242 \cdot k'_{2b} \cdot k'_{2s} + 0.091 \cdot k'_{2b} \cdot k'_{3s} + 0.053 \cdot k'_{3b} \cdot k'_{2s} + 3.509 \cdot \frac{d_1}{d_2} \\
 &- 0.955 \cdot \left( \frac{d_1}{d_2} - 1 \right)^2 .
 \end{aligned}$$

- The  $R^2$  is 0.95, and the mean square accuracy of this approximation is 16%.

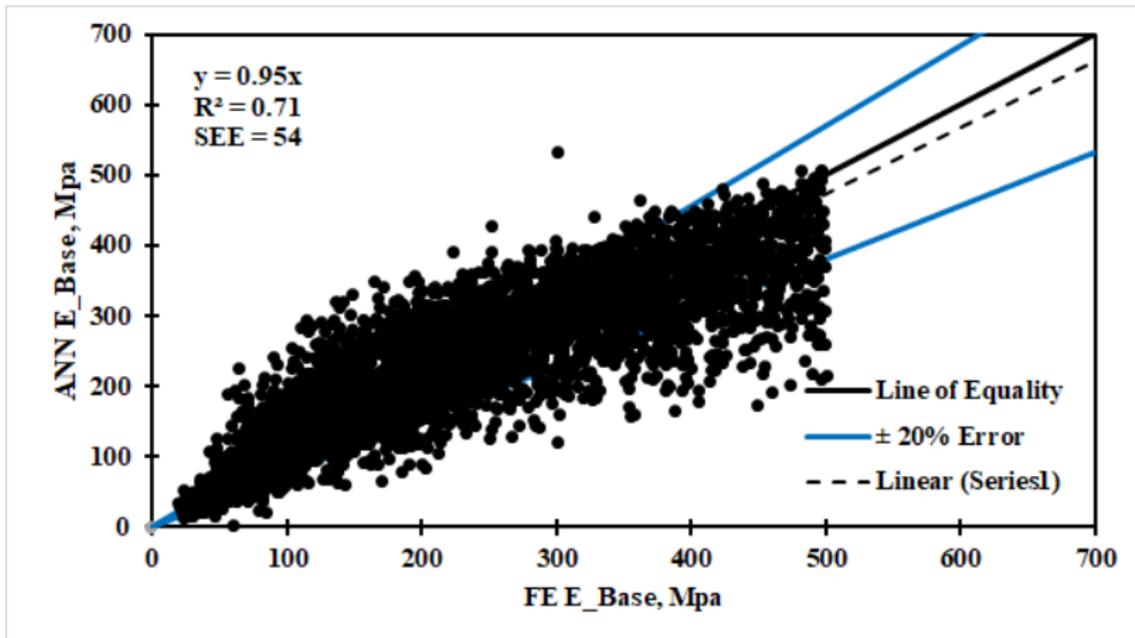
- For the **300 mm** cases, we have

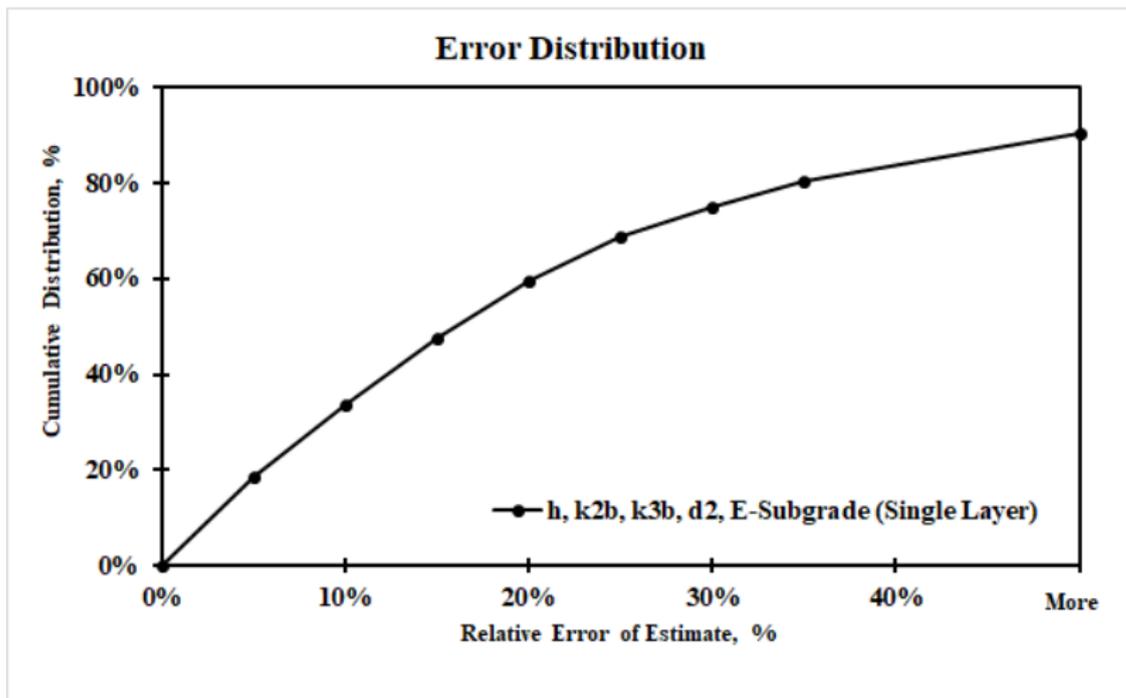
$$\begin{aligned}
 \ln(d_2 \cdot E) &= 3.870 + 0.380 \cdot k'_{2b} + 0.348 \cdot k'_{3b} + 0.408 \cdot k'_{2s} + 0.196 \cdot k'_{3s} \\
 &+ 0.078 \cdot k'_{2b} \cdot k'_{3b} + 0.037 \cdot (k'_{3b})^2 - 0.177 \cdot (k'_{2s})^2 - 0.160 \cdot k'_{2s} \cdot k'_{3s} \\
 &- 0.029 \cdot (k'_{3s})^2 + 0.138 \cdot k'_{2b} \cdot k'_{2s} + 0.065 \cdot k'_{2b} \cdot k'_{3s} + 0.069 \cdot k'_{3b} \cdot k'_{2s} \\
 &+ 0.041 \cdot k'_{3b} \cdot k'_{3s} + 1.656 \cdot \frac{d_1}{d_2} - 0.294 \cdot \left( \frac{d_1}{d_2} - 1 \right)^2 .
 \end{aligned}$$

- The  $R^2$  is 0.96, and the mean square accuracy of this approximation is 11%.

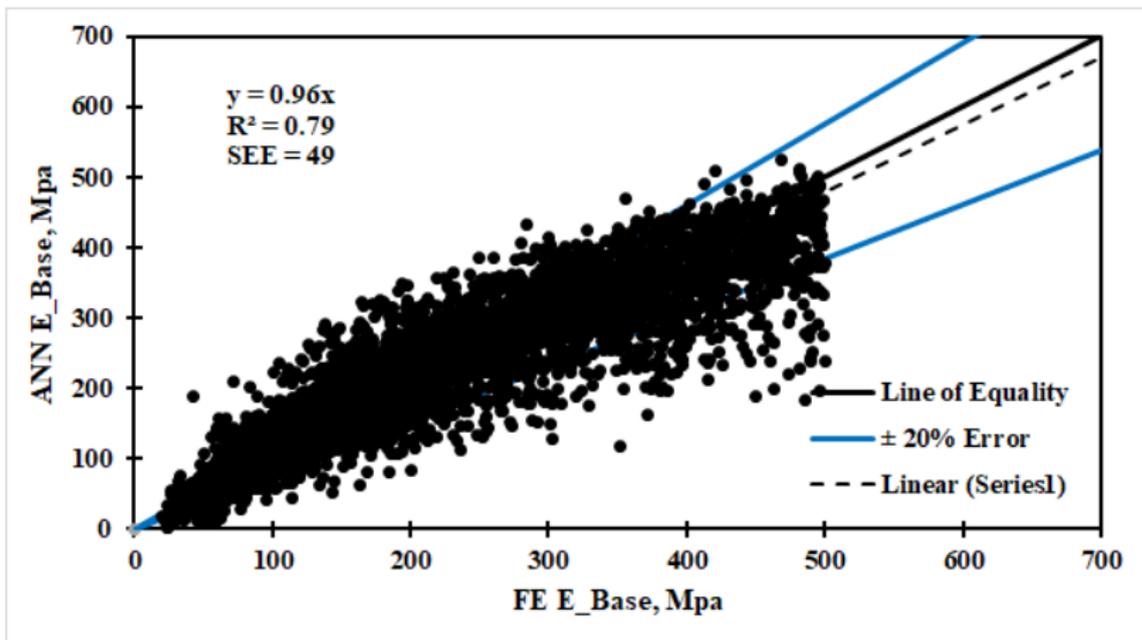
- As it was mentioned earlier, to estimate the elastic modulus  $E_1$  of the subgrade;
  - we do not really need to know the values of the parameters  $k'_2$  and  $k'_3$  corresponding to the subgrade,
  - it is sufficient to know the corresponding displacement  $d_1$ .
- As a result, practitioners do not need to estimate these parameters when compacting the subgrade.
- It is therefore reasonable to also consider a realistic scenario in which:
  - instead of the values  $d_1$ ,  $k'_{2s}$ , and  $k'_{3s}$ ,
  - we only know the estimate  $E_1$ .

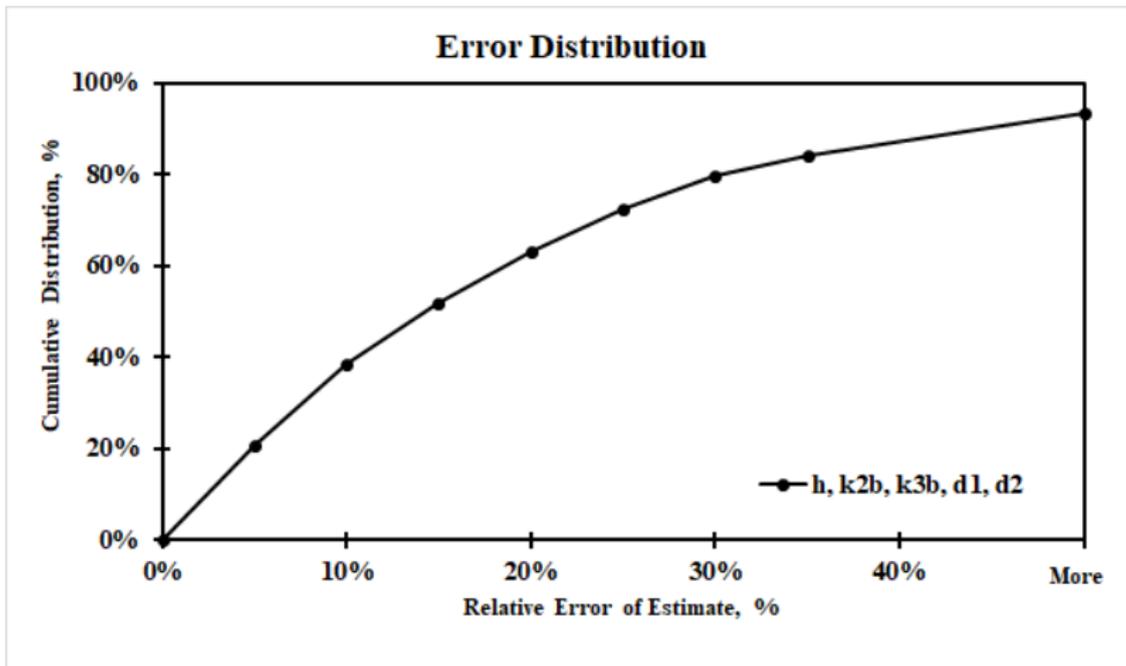
- Another reason why such a scenario is needed is that:
  - while the properties of the base are reasonably well known,
  - the properties of the subgrade may vary greatly from site to site.
- In such scenario,
  - in addition to the displacement  $d_2$ , and the parameters  $h$ ,  $k'_{2b}$ , and  $k'_{3b}$  that describe the base,
  - we have an estimate  $E_1$  for the elastic modulus of the subgrade.
  - Multiple neural networks were trained to estimate the modulus  $E_2$ .
- The results are as follows:





- Slightly more accurate estimates can be obtained if we take into account that the above formula for the dependence of  $E_1$  on  $d_1$ , while reasonably accurate, is still approximate.
- Therefore, we can get better estimates if instead of using the estimate  $E_1$ , we use the displacement  $d_1$ ; this way, we avoid the effect of the above inaccuracy.
- In other words, as inputs for estimating  $E_2$ , we use  $d_2, h, k'_{2b}, k'_{3b}$ , and the displacement  $d_1$ .
- The resulting estimates of training the corresponding neural network model are presented here:





- Even more accurate estimates for  $E_2$  can be obtained if we use the actual values  $E_1^{\text{act}}$  of the subgrade's representative modulus  $E_1$  instead of  $d_1$  or the  $d_1$ -based estimate for  $E_1$ .
- In this case, to estimate  $E_2$ , we use the values  $d_2$ ,  $h$ ,  $k'_{2b}$ ,  $k'_{3b}$ , and  $E_1^{\text{act}}$ .
- The results of the corresponding neural network model are presented here:

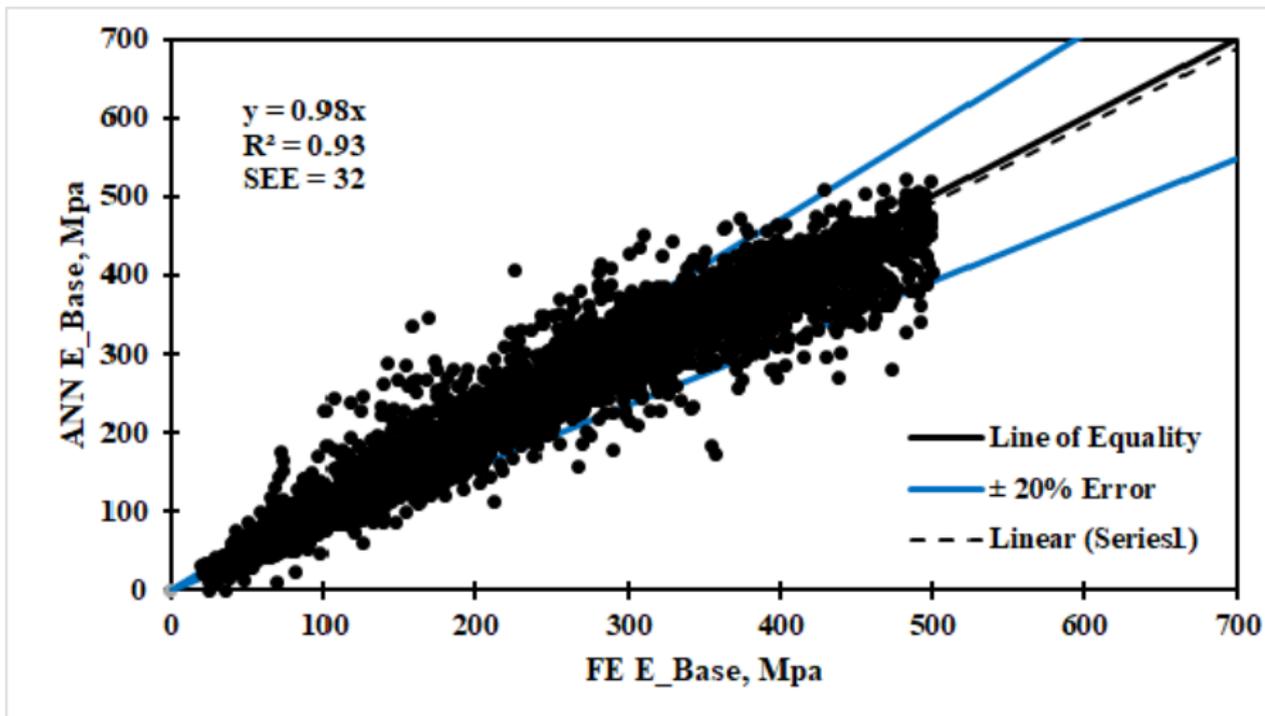


Figure: Case when we use the actual value  $E_1^{act}$

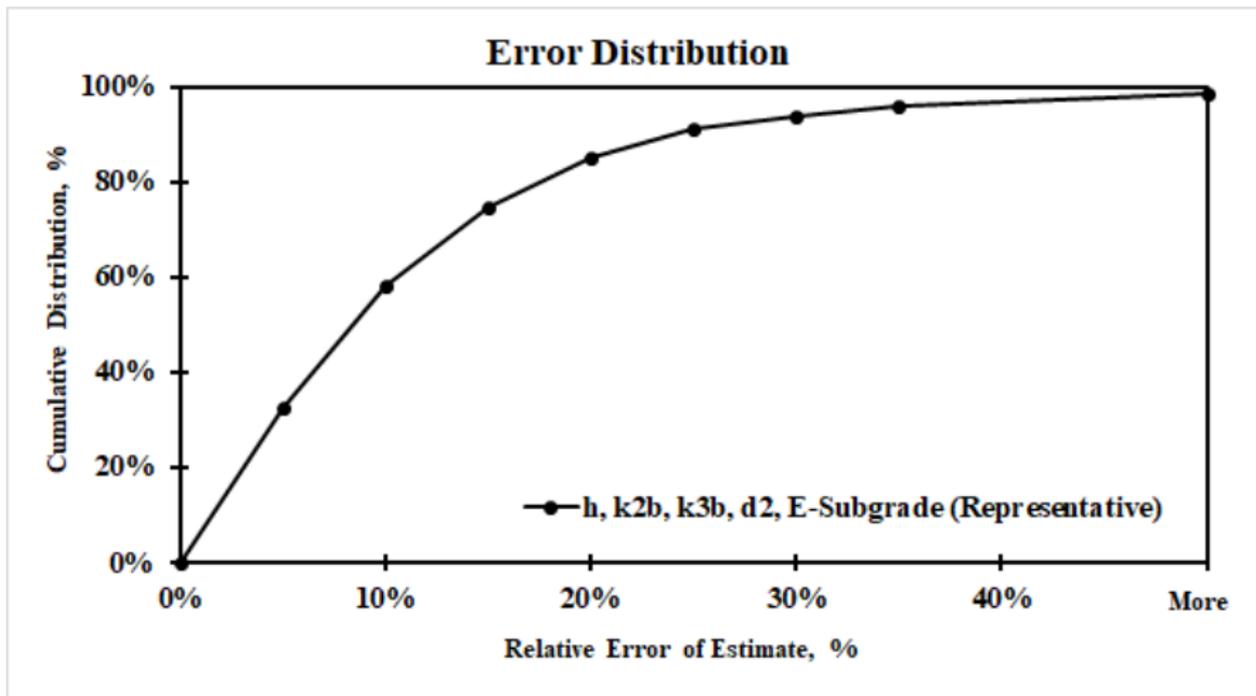


Figure: Case when we use the actual value  $E_1^{\text{act}}$

- We combined the distribution of the estimation errors of all three models in a single graph.

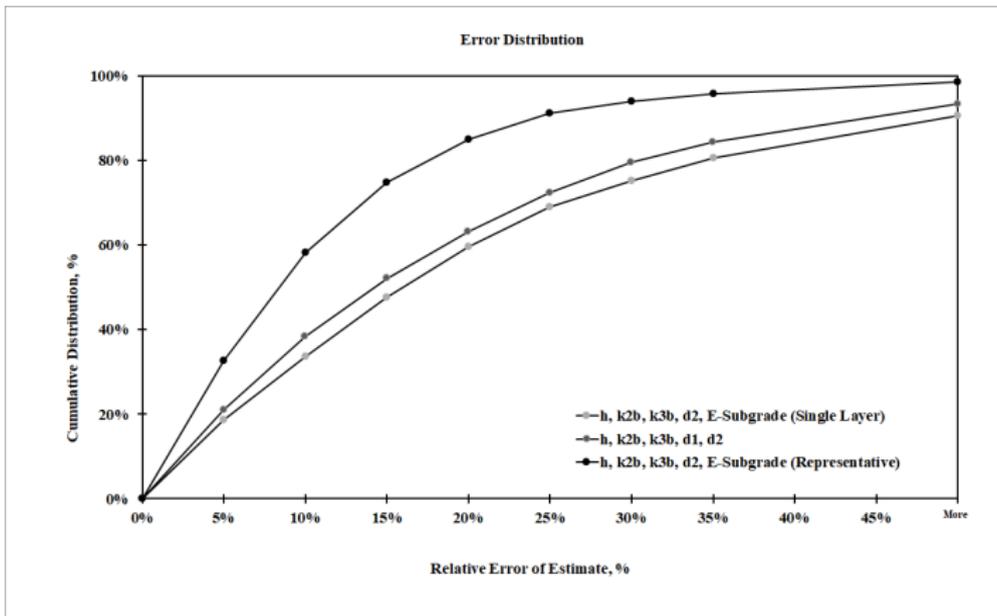


Figure: Comparative accuracy of three neural network models

- All the simulations assume that both the subgrade and the base layers are homogeneous.
- In practice, the mechanical properties of the subgrade and of the base can randomly change by 20-25%, so it is sufficient to have accuracy 20-25%.
- It turns out that with this accuracy, we can have

$$\ln(d_2^{\text{dyn}} \cdot E^{\text{dyn}}) = a_0 + a_1 \cdot \ln(d_2^{\text{stat}} \cdot E^{\text{stat}}).$$

- For **150 mm**,  $a_0 = 0.96$  and  $a_1 = 0.81$ , accuracy is 17%.
- For **300 mm**,  $a_0 = 1.68$ ,  $a_1 = 0.69$ , accuracy 16%.
- Thus, time-consuming dynamical simulations are not needed, and we can reconstruct their results based on static cases.

# *Part Three*



---

## Theoretical Explanation of Ooi's Formula

- Experimental comparison shows that the best description is provided by the formula

$$E = k'_1 \cdot \left( \frac{\theta}{P_a} + 1 \right)^{k'_2} \cdot \left( \frac{\tau_{\text{oct}}}{P_a} + 1 \right)^{k'_3},$$

where

$$\theta = \sigma_1 + \sigma_2 + \sigma_3$$

and

$$\tau_{\text{oct}} = \frac{1}{3} \cdot \sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2}.$$

- How can we explain this formula?



- Computers process numerical values of different quantities.
- A numerical value of a quantity depends:
  - on the choice of a measuring unit, and
  - on the choice of the starting point.
- For example: we can describe the height of the same person as 1.7 m or 170 cm.
  - 14.00 by El Paso time is 15.00 by Austin time.
  - Reason: the starting points – midnights (00.00) – differ by an hour.
  - The choice of a measuring unit is rather arbitrary.



## Main Idea (cont-d)

- It is reasonable to require that the fundamental physical formulas not depend
  - on the choice of a measuring unit and
  - if appropriate – on the choice of the starting point.
- We do not expect that, e.g., Newton's laws look differently if we use meters or feet.
- If we change the units, then we may need to adjust units of related quantities.
  - For example, if we replace m with cm, then we need to replace m/sec with cm/sec when measuring velocity.
- However, once the appropriate adjustments are made, we expect the formulas to remain the same.



## Not All Physical Quantities Allow Both Changes

- Some quantities have a fixed starting point.
- Examples:
  - while we can choose an arbitrary starting point for time,
  - for distance, 0 distance seems to be a reasonable starting point.
- As a result:
  - while the change of a measuring unit makes sense for most physical quantities,
  - the change of a starting point only makes sense for some of them.
- A physics-based analysis is needed to decide whether this change makes physical sense.

- **Case:** we replace the original measuring unit with a new unit which is  $a$  times smaller.  
 $x' = a \cdot x$ .
  - *Example:* 1.7 m is  $x' = a \cdot x = 100 \cdot 1.7 = 170$  cm.
- **Case:** we replace the original starting point by a new one which is  $b$  earlier (or smaller).  
 $x' = x + b$ .
- 14 hr in El Paso is  $x' = x + b = 14 + 1 = 15$  in Austin.
- **General case:** we can change both the measuring unit and the starting point.  
Then,  $x \rightarrow a \cdot x + b$ .



## How Elastic Modulus $E$ Depends on the Bulk Stress $\theta$

- **For  $E$** , there is a clear starting point  $E = 0$ , in which strain does not cause any stress.
- So, for  $E$ , only a change in a measuring unit makes physical sense.
- **For  $\theta$** , a change in starting point is also possible:
  - we can only count the external stress,
  - or we can explicitly take atmospheric pressure into account.
- It turns out that Ooi's formula can be derived from these invariances.

# *Part Four*



---

## Safety Factors in Soil and Pavement Engineering: Theoretical Explanation of Empirical Data



# What Is a Safety Factor

- Models are approximations to reality.
- To describe a complex real-life process by a feasible model:
  - we find the most important factors affecting the process and
  - we model them.
- The ignored factors are smaller than the factors that we take into account; however:
  - they still need to be taken into account
  - if we want to provide guaranteed bounds for the desired quantities.
- To take these small factors into account, engineers multiply the results of the model by a constant.
- This constant is known as the **safety factor**.



# Safety Factors in Soil and Pavement Engineering

- In many applications, a safety factor is 2 or smaller.
- However, in soil and pavement engineering, the situation is different.
- Researchers compared:
  - the elastic modulus predicted by the corresponding model and
  - the modulus measured by Light Weight Deflectometer.
- This comparison showed that:
  - to provide guaranteed bounds,
  - we need a safety factor of 4.
- How can we explain this?

- Let  $\Delta$  be the model's estimate.
- When designing the model, we did not take into account some factors. Let's denote the effect of the largest of these factors by  $\Delta_1$ .
- The factors that we ignored are smaller than the one we took into account, so:

$$\Delta_1 < \Delta, \text{ i.e., } \Delta_1 \in (0, \Delta).$$

- We do not have any reason to assume that any value from the interval  $(0, \Delta)$  is more frequent than others. Thus, it makes sense to assume that  $\Delta_1$  is uniformly distributed on  $(0, \Delta)$ .
- Then, the average value of  $\Delta_1$  is  $\frac{\Delta}{2}$ .
- The next smallest factor  $\Delta_2$  is smaller than  $\Delta_1$ .

- The same arguments shows that its average value of  $\Delta_2$  is  $\frac{\Delta_1}{2}$ , i.e.,

$$\begin{aligned}\Delta_1 &= 2^{-1} \cdot \Delta \\ \Delta_2 &= 2^{-1} \cdot \Delta_1 \\ &= 2^{-2} \cdot \Delta\end{aligned}$$

Therefore, for each  $k > 0$

$$\Delta_k = 2^{-k} \cdot \Delta$$

- Hence the overall estimate is

$$\begin{aligned}\Delta + \Delta_1 + \dots + \Delta_k + \dots &= \Delta + 2^{-1} \cdot \Delta + \dots + 2^{-k} \cdot \Delta + \dots \\ &= 2\Delta.\end{aligned}$$

## A Similar Explanation for the Safety Factor of 4

- Empirical data shows that for soil and pavement engineering, 2 is not enough.
- This means that  $\Delta_1$  should be larger than our estimate  $\frac{\Delta_1}{2}$ :  $\Delta_1 \in (\frac{\Delta}{2}, \Delta)$ .

$$\Delta_1 = \frac{3}{4} \cdot \Delta$$

$$\Delta_2 = \left(\frac{3}{4}\right)^2 \cdot \Delta$$

Therefore, for each  $k > 0$

$$\Delta_k = \left(\frac{3}{4}\right)^k \cdot \Delta$$

and thus,

$$\begin{aligned} \Delta + \Delta_1 + \dots + \Delta_k + \dots &= \Delta \cdot (1 + 3/4 + \dots + (3/4)^k + \dots) \\ &= \Delta / (1 - 3/4) \\ &= 4\Delta. \end{aligned}$$

# *Part Five*



How Many Monte-Carlo Simulations Are Needed?



## How Many Monte-Carlo Simulations Are Needed?

- We provide a partial answer to the question of how many Monte-Carlo simulations are needed.
- Namely, we provide this answer for the case of interval uncertainty.
- A recent research used Monte-Carlo technique to compare algorithms for smart electric grid.
- The study computed ranges (intervals) for different quantities.
- This study shows that we need  $\approx 500$  simulations to reach 5% accuracy.
- In this dissertation, we provide a theoretical explanation for these empirical results.

# *Part Six*



Why 70/30 Relation Between Training and Testing Sets



## Why 70/30 Relation Between Training and Testing Sets?

- Overfitting is when the model closely follows all the available data – but is lousy in predictions.
- To avoid this, it is important to divide the data into the **training set** and the **testing set**.
  - We first train our model on the training set.
  - Then we use the data from the testing set to gauge the accuracy of the resulting model.
- Empirical studies show that the best results are obtained if we use 20-30% of the data for testing. The remaining 70-80% of the data is for training.
- We provide a possible explanation for this empirical result.

# *Part Seven*



---

## How to Minimize Relative Error

## How to Minimize Relative Error?

- In many problems, there is a need to find the parameters of a dependence from the experimental data.
- There exist several software packages that find the values for these parameters.
- Usually, we minimize the the **mean square value** of the **absolute approximation error**.
- For example, in the linear case, we minimize the sum

$$\sum_{k=1}^K \left( y^{(k)} - \sum_{j=1}^m c_j \cdot f_j \left( x_1^{(k)}, \dots, x_n^{(k)} \right) \right)^2 .$$

- In practice, however, we are often interested in minimizing the **relative approximation error**.

- It is desirable to use absolute-value software to minimize relative errors.
- We analyze this problem.
- For the **linear case**, our recommendation is to minimize the sum

$$\sum_{k=1}^K \left( 1 - \sum_{j=1}^m c_j \cdot \frac{f_j(x_1^{(k)}, \dots, x_n^{(k)})}{y^{(k)}} \right)^2 .$$

- A similar recommendation works in the **non-linear case**.

# *Part Eight*



## How to Best Apply Neural Networks

- The main objectives of geosciences is:
  - to find the current state of the Earth – i.e., solve the corresponding *inverse problems* – and
  - to use this knowledge for predicting the future events, such as earthquakes and volcanic eruptions.
- In both inverse and prediction problems, often, machine learning techniques are very efficient.
- At present, the most efficient machine learning technique is **neural networks**.
- To speed up this training, the current machine learning algorithms use **dropout techniques**:
  - they train several sub-networks on different portions of data, and
  - then "average" the results.



- A natural idea is to use **arithmetic mean** for this “averaging”.
- However, empirically, **geometric mean** works much better.
- In this dissertation, we explain the empirical efficiency of geometric mean.
- This explanation uses the same independence-on-measuring units as in explaining Ooi’s formula.

# *Part Nine*



What Is the Optimal Bin Size of a Histogram?



# What Is the Optimal Bin Size of a Histogram?

- A natural way to estimate the probability density function from the sample is to use **histograms**.
- The accuracy of the estimate depends on the size of the histogram's bins  $h$ .
- There exist heuristic rules for selecting the bin size.
- The probability density  $\rho(x)$  changes from 0 to 1 then from 1 to 0 on an interval of width  $s$ . Therefore, its average rate of change is  $1/(s/2)$ .
- In a bin of size  $h$ , we approximate each value  $\rho(x)$  by a value at midpoint.
- The largest distance from midpoint is  $h/2$ .

# What Is the Optimal Bin Size of a Histogram?

- Thus, the relative change is  $(h/2)/(s/2) = \frac{h}{s}$ .
- On the other hand, in each bin, we have  $m = n \cdot \frac{h}{s}$  points.
- According to statistics, estimates based on  $m$  points has accuracy  $\frac{1}{\sqrt{m}}$ .
- Minimizing the overall error  $\frac{h}{s} + \frac{1}{\sqrt{m}}$
- Therefore:
$$h_{\text{opt}} = \text{const} \cdot s \cdot n^{-1/3}$$
which is exactly the empirically **optimal bin size**.
- Thus, we have theoretically justified this empirical choice.

# *Part Ten*



---

## Conclusions

- It is desirable to speed up the quality assessment of the newly built roads. Thus, we need to measure the road's stiffness in real time, as the road is being built.
- This is the main idea behind **intelligent compaction**, when:
  - accelerometers and other measuring instruments are attached to the roller, and
  - the results of the corresponding measurements are used to gauge the road's stiffness.
- **The main challenge:** formulas for estimating the road's stiffness are complicated.
- It is a complex system of partial differential equations which are difficult to solve in real time.

- It is therefore desirable to come up with easier-to-compute algorithms.
- The **main task** of this dissertation was the design of such algorithms.
- As a solution to this task, we propose both:
  - most-easy-to-compute analytical expressions and
  - somewhat more complex (but still easy to compute) neural network models.
- We also provide a theoretical explanations for:
  - the empirical formulas used to describe the road dynamics, and
  - the empirical safety factor that related the simulation results with actual road measurements.

- In the process of solving the main task, we have also solved several auxiliary tasks, explaining:
  - how many simulations are needed,
  - what is the best relation between training and testing sets,
  - how to take into account that we often need to minimize relative error,
  - how to best apply neural networks, and
  - what is the optimal bin size in a histogram.
- We hope that both our solution of the main tasks and our solutions to the auxiliary tasks will be useful.



# Acknowledgments

- I am very thankful to Drs. Laura Serpa and Vladik Kreinovich my Committee Co-Chair.
- I am also very grateful to all the members of my committee:
  - ▶ Soheil Nazarian,
  - ▶ Hector Gonzalez,
  - ▶ and last but not least, Aaron Velasco.
- Many thanks to all for your help and support.